

Table 2 Suggested prediction methods to use for a given set of available input parameters per each examined soil hydraulic property)<sup>a</sup>.

| Reference number of model indicated in Table 1 | Predicted soil hydraulic property                | Type of model | Prediction model  |
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| (1)  | $\theta_s$<br>/ cm <sup>3</sup> cm <sup>-3</sup> | RT            | <p>Rule 1<br/>IF FAO_MOD=coarse,medium,medium fine AND T/S=sub<br/><math>\theta_s = 0.416</math></p> <p>Rule 2<br/>IF FAO_MOD=coarse,medium,medium fine AND T/S=top<br/><math>\theta_s = 0.467</math></p> <p>Rule 3<br/>IF FAO_MOD=fine<br/><math>\theta_s = 0.475</math></p> <p>Rule 4<br/>IF FAO_MOD=very fine<br/><math>\theta_s = 0.564</math></p> <p>Rule 5<br/>IF FAO_MOD=organic<br/><math>\theta_s = 0.847</math></p> |
| (2)  | $\theta_s$<br>/ cm <sup>3</sup> cm <sup>-3</sup> | RT            | <p>Rule 1<br/>IF FAO_MOD=coarse,medium,medium fine AND OC &lt; 0.11<br/><math>\theta_s = 0.365</math></p> <p>Rule 2<br/>IF OC ≥ 0.11 AND OC &lt; 0.17<br/><math>\theta_s = 0.393</math></p> <p>Rule 3<br/>IF OC ≥ 0.17 AND OC &lt; 1.74 AND FAO_MOD=coarse<br/><math>\theta_s = 0.399</math></p> <p>Rule 4<br/>IF FAO_MOD=medium AND OC ≥ 0.90 AND OC &lt; 1.74 AND T/S=sub<br/><math>\theta_s = 0.389</math></p>             |

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|  |  | <p>Rule 5<br/>IF FAO_MOD=medium AND OC&gt;=0.90 AND OC&lt;1.74 AND T/S=top<br/><math>\theta_s = 0.435</math></p> <p>Rule 6<br/>IF OC&gt;=0.17 AND OC&lt;0.90 AND FAO_MOD=medium<br/><math>\theta_s = 0.427</math></p> <p>Rule 7<br/>IF OC&gt;=0.17 AND OC&lt;0.32 AND FAO_MOD=medium fine<br/><math>\theta_s = 0.412</math></p> <p>Rule 8<br/>IF FAO_MOD=medium fine AND OC&gt;=0.32 AND OC&lt;1.74<br/><math>\theta_s = 0.453</math></p> <p>Rule 9<br/>IF FAO_MOD=fine,very fine AND OC&lt;0.63<br/><math>\theta_s = 0.434</math></p> <p>Rule 10<br/>IF OC&gt;=0.63 AND OC&lt;1.74 AND FAO_MOD=fine<br/><math>\theta_s = 0.482</math></p> <p>Rule 11<br/>IF OC&gt;=0.63 AND OC&lt;1.74 AND FAO_MOD=very fine<br/><math>\theta_s = 0.557</math></p> <p>Rule 12<br/>IF OC&gt;=1.74 AND OC&lt;2.21 AND FAO_MOD=coarse,fine,medium<br/><math>\theta_s = 0.461</math></p> <p>Rule 13<br/>IF OC&gt;=3.79 AND OC&lt;4.64 AND T/S=top AND FAO_MOD=fine<br/><math>\theta_s = 0.377</math></p> <p>Rule 14<br/>IF OC&lt;3.79 AND OC&gt;=1.74 AND T/S=top AND FAO_MOD=fine<br/><math>\theta_s = 0.471</math></p> <p>Rule 15<br/>IF OC&gt;=2.21 AND OC&lt;4.64 AND T/S=top AND FAO_MOD=coarse,medium<br/><math>\theta_s = 0.488</math></p> |
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|  |  | <p>Rule 16<br/>IF OC&gt;= 2.21 AND OC&lt;4.64 AND T/S=sub AND FAO_MOD=coarse,medium<br/><math>\theta_s = 0.477</math></p> <p>Rule 17<br/>IF OC&gt;= 2.21 AND OC&lt;4.64 AND T/S=sub AND FAO_MOD=fine<br/><math>\theta_s = 0.570</math></p> <p>Rule 18<br/>IF FAO_MOD=medium fine AND OC&lt; 3.11 AND OC&gt;=1.74<br/><math>\theta_s = 0.502</math></p> <p>Rule 19<br/>IF FAO_MOD=medium fine AND OC&gt;=3.11 AND OC&lt;4.64<br/><math>\theta_s = 0.596</math></p> <p>Rule 20<br/>IF OC&gt;=1.74 AND OC&lt;4.64 AND FAO_MOD=very fine<br/><math>\theta_s = 0.628</math></p> <p>Rule 21<br/>IF OC&gt;=4.64 AND OC&lt; 7.85 AND FAO_MOD=coarse,medium<br/><math>\theta_s = 0.531</math></p> <p>Rule 22<br/>IF FAO_MOD=coarse,medium AND OC&gt;=7.85 AND OC&lt;10.89<br/><math>\theta_s = 0.594</math></p> <p>Rule 23<br/>IF OC&gt;=4.64 AND OC&lt;10.89 AND FAO_MOD=fine,medium fine,very fine<br/><math>\theta_s = 0.625</math></p> <p>Rule 24<br/>IF OC&gt;=10.89 AND OC&lt; 17.33<br/><math>\theta_s = 0.676</math></p> <p>Rule 25<br/>IF OC&gt;=17.33 AND OC&lt;30.34<br/><math>\theta_s = 0.771</math></p> <p>Rule 26<br/>IF OC&gt;=30.34 AND OC&lt; 48.63<br/><math>\theta_s = 0.851</math></p> |
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|     |   |    | <p>Rule 27<br/> IF OC&gt;=48.63<br/> <math>\theta_s = 0.914</math></p>   |
| (3) | $\theta_s$<br>/cm <sup>3</sup> cm <sup>-3</sup> | RT | <p>Rule 1<br/> IF USDA=S,SCL AND T/S=sub<br/> <math>\theta_s = 0.381</math></p> <p>Rule 2<br/> IF USDA=SL AND T/S=sub<br/> <math>\theta_s = 0.407</math></p> <p>Rule 3<br/> IF USDA=CL,L,LS,SiL AND T/S=sub<br/> <math>\theta_s = 0.428</math></p> <p>Rule 4<br/> IF USDA=CL,L,LS,S,SCL,SiL,SL AND T/S=top<br/> <math>\theta_s = 0.465</math></p> <p>Rule 5<br/> IF USDA=Si,SiC,SiCL<br/> <math>\theta_s = 0.470</math></p> <p>Rule 6<br/> IF USDA=C,SC<br/> <math>\theta_s = 0.520</math></p> <p>Rule 7<br/> IF USDA=O AND T/S=top<br/> <math>\theta_s = 0.767</math></p> <p>Rule 8<br/> IF USDA=O AND T/S=sub<br/> <math>\theta_s = 0.865</math></p> |
| (4) | $\theta_s$<br>/cm <sup>3</sup> cm <sup>-3</sup> | RT | <p>Rule 1<br/> IF OC&lt; 1.74 AND OC&gt;=0.33 AND Sa&lt; 37.37 AND Sa&gt;=5.39 AND CL&lt; 49.25<br/> <math>\theta_s = 0.451</math></p> <p>Rule 2<br/> IF OC&lt; 0.90 AND OC&gt;=0.11 AND Sa&gt;=37.37 AND T/S=sub<br/> <math>\theta_s = 0.399</math></p>   |

Rule 3

IF OC<0.33 AND Sa<37.37

$\theta_s = 0.406$

Rule 4

IF OC>=2.78 AND OC<4.64 AND Cl<52.15 AND Si<59.03 AND Sa>=4.05

$\theta_s = 0.490$

Rule 5

IF OC>=1.74 AND OC<2.78 AND Cl<52.15 AND Si<59.03 AND Sa>=4.05

$\theta_s = 0.461$

Rule 6

IF OC<1.74 AND OC>=0.90 AND Sa>=37.37 AND T/S=sub

$\theta_s = 0.375$

Rule 7

IF OC<1.74 AND OC>=0.11 AND Sa>=37.37 AND T/S=top

$\theta_s = 0.418$

Rule 8

IF OC<0.11 AND Sa>=37.37 AND Cl<11.55

$\theta_s = 0.374$

Rule 9

IF OC>=4.64 AND OC<7.85 AND Sa>=29.51

$\theta_s = 0.531$

Rule 10

IF OC<1.74 AND OC>=0.63 AND Sa<37.37 AND Cl>=49.25

$\theta_s = 0.532$

Rule 11

IF OC<0.11 AND Sa>=37.37 AND Cl>=11.55

$\theta_s = 0.328$

Rule 12

IF OC>=1.74 AND OC<4.64 AND Cl<52.15 AND Si>=59.03

$\theta_s = 0.522$

Rule 13

IF OC<1.74 AND OC>=0.33 AND Sa<5.39 AND Cl<49.25

THS=0.499

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|     |   |     | <p>Rule 14<br/>IF OC&lt;0.63 AND OC&gt;=0.33 AND Sa&lt;37.37 AND Cl&gt;=49.25<br/><math>\theta_s = 0.463</math></p> <p>Rule 15<br/>IF OC&gt;=1.74 AND OC&lt;4.64 AND Cl&gt;=52.15<br/>THS=0.593</p> <p>Rule 16<br/>IF OC&gt;=4.64 AND OC&gt;=7.85 AND Sa&gt;=29.51<br/><math>\theta_s = 0.595</math></p> <p>Rule 17<br/>IF OC&gt;=3.21 AND OC&lt;4.64 AND Cl&lt;52.15 AND Si&lt;59.03 AND Sa&lt;4.05<br/><math>\theta_s = 0.382</math></p> <p>Rule 18<br/>IF OC&gt;=4.64 AND Sa&lt;29.51 AND T/S=sub<br/><math>\theta_s = 0.695</math></p> <p>Rule 19<br/>IF OC&gt;=4.64 AND Sa&lt;29.51 AND T/S=top<br/><math>\theta_s = 0.587</math></p> <p>Rule 20<br/>IF OC&gt;=1.74 AND OC&lt;3.21 AND Cl&lt;52.15 AND Si&lt;59.03 AND Sa&lt;4.05<br/><math>\theta_s = 0.525</math></p> |
| (5) | $\theta_s$<br>/ cm <sup>3</sup> cm <sup>-3</sup>    | Lrt | $\theta_s = 0.6819 - 0.06480 * (1/(OC+1)) - 0.1190 * (1/(OC+1)) * BD^2 - 0.02683 * BD^2 + 0.001489 * T/S + 0.0008031 * T/S * BD^2 + 0.02321 * Cl + 0.01908 * Cl * T/S - 0.001109 * Si - 0.0002315 * Si * Cl - 0.0001997 * Si * BD^2 - 0.0001068 * Cl * BD^2$   |
| (6) | $\theta_s$<br>/ cm <sup>3</sup> cm <sup>-3</sup>    | Lrt | $\theta_s = 0.5653 - 0.07918 * BD^2 + 0.001671 * pH^2 + 0.0005438 * Cl + 0.001065 * Cl * pH^2 + 0.06836 * Si - 0.00001381 * Si * Cl - 0.00001270 * BD^2 * pH^2 - 0.0004784 * Si * BD^2 - 0.0002836 * Cl * BD^2 + 0.0004158 * T/S - 0.01686 * T/S * BD^2 - 0.0003541 * Si * T/S - 0.0003152 * T/S * pH^2$   |
| (7) | $\theta_{fc}$<br>/ cm <sup>3</sup> cm <sup>-3</sup> | RT  | <p>Rule 1<br/>IF FAO_MOD=coarse AND T/S=sub<br/><math>\theta_{fc} = 0.157</math></p> <p>Rule 2<br/>IF FAO_MOD=coarse AND T/S=top<br/><math>\theta_{fc} = 0.199</math></p> <p>Rule 3<br/>IF FAO_MOD=medium AND T/S=sub<br/><math>\theta_{fc} = 0.280</math></p>   |

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|     |  |    | <p>Rule 4<br/>IF FAO_MOD=medium AND T/S=top<br/><math>\theta_{FC} = 0.308</math></p> <p>Rule 5<br/>IF FAO_MOD=medium fine<br/><math>\theta_{FC} = 0.326</math></p> <p>Rule 6<br/>IF FAO_MOD=fine, very fine<br/><math>\theta_{FC} = 0.362</math></p> <p>Rule 7<br/>IF FAO_MOD=organic<br/><math>\theta_{FC} = 0.575</math></p>  |
| (8) | $\theta_{FC}$<br>/ $\text{cm}^3\text{cm}^{-3}$ | RT | <p>Rule 1<br/>IF USDA=S<br/><math>\theta_{FC} = 0.094</math></p> <p>Rule 2<br/>IF USDA=LS<br/><math>\theta_{FC} = 0.165</math></p> <p>Rule 3<br/>IF USDA=Si,SL<br/><math>\theta_{FC} = 0.236</math></p> <p>Rule 4<br/>IF USDA=SC,SCL AND T/S=sub<br/><math>\theta_{FC} = 0.255</math></p> <p>Rule 5<br/>IF USDA=SC,SCL AND T/S=top<br/><math>\theta_{FC} = 0.309</math></p> <p>Rule 6<br/>IF USDA=L,SiL<br/><math>\theta_{FC} = 0.312</math></p> <p>Rule 7<br/>IF USDA=CL,SiCL AND T/S=sub<br/><math>\theta_{FC} = 0.321</math></p> |

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|      |  |     | <p>Rule 8<br/>IF USDA=CL,SiCL AND T/S=top<br/><math>\theta_{FC} = 0.355</math></p> <p>Rule 9<br/>IF USDA=C,SiC<br/><math>\theta_{FC} = 0.372</math></p> <p>Rule 10<br/>IF USDA=O AND T/S=top<br/><math>\theta_{FC} = 0.503</math></p> <p>Rule 11<br/>IF USDA=O AND T/S=sub<br/><math>\theta_{FC} = 0.596</math></p>  |
| (9)  | $\theta_{FC}$<br>/ $\text{cm}^3\text{cm}^{-3}$ | Lrt | $\theta_{FC} = 0.2449 - 0.1887 * (1/(OC+1)) + 0.004527 * Cl + 0.001535 * Si + 0.001442 * Si * (1/(OC+1)) - 0.00005110 * Si * Cl + 0.0008676 * Cl * (1/(OC+1))$   |
| (10) | $\theta_{WP}$<br>/ $\text{cm}^3\text{cm}^{-3}$ | RT  | <p>Rule 1<br/>IF FAO_MOD=coarse<br/><math>\theta_{WP} = 0.069</math></p> <p>Rule 2<br/>IF FAO_MOD=medium<br/><math>\theta_{WP} = 0.140</math></p> <p>Rule 3<br/>IF FAO_MOD=medium fine<br/><math>\theta_{WP} = 0.163</math></p> <p>Rule 4<br/>IF FAO_MOD=fine, organic AND T/S=top<br/><math>\theta_{WP} = 0.233*</math></p> <p>Rule 5<br/>IF FAO_MOD=fine, organic AND T/S=sub<br/><math>\theta_{WP} = 0.268</math></p> <p>Rule 6<br/>IF FAO_MOD=very fine<br/><math>\theta_{WP} = 0.325</math></p> |
| (11) | $\theta_{WP}$                                  | RT  | Rule 1   |



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|      | / cm <sup>3</sup> cm <sup>-3</sup>                    |     | <p>IF USDA=LS,S,Si<br/> <math>\theta_{WP} = 0.050</math></p> <p>Rule 2<br/> IF USDA=SL<br/> <math>\theta_{WP} = 0.100</math></p> <p>Rule 3<br/> IF USDA=L,SiL<br/> <math>\theta_{WP} = 0.136</math></p> <p>Rule 4<br/> IF USDA=SCL<br/> <math>\theta_{WP} = 0.164</math></p> <p>Rule 5<br/> IF USDA=CL,SC,SiCL<br/> <math>\theta_{WP} = 0.211</math></p> <p>Rule 6<br/> IF USDA=C,O,SiC AND T/S=top<br/> <math>\theta_{WP} = 0.251</math></p> <p>Rule 7<br/> IF USDA=C,O,SiC AND T/S=sub<br/> <math>\theta_{WP} = 0.292</math></p> |
| (12) | $\theta_{WP}$<br>/ cm <sup>3</sup> cm <sup>-3</sup>   | Lrt | $\theta_{WP} = 0.09878 + 0.002127 * Cl - 0.0008366 * Si - 0.07670 * Si * Cl + 0.00003853 * (1/(OC+1)) + 0.002330 * Cl * (1/(OC+1)) + 0.0009498 * Si * (1/(OC+1))$  |
| (13) | $\log_{10}(K_s)$<br>/ $\log_{10}(\text{cm day}^{-1})$ | RT  | <p>Rule 1<br/> IF T/S=sub AND FAO_MOD=coarse,medium,medium fine,organic<br/> <math>\log_{10}(K_s) = 0.77</math></p> <p>Rule 2<br/> IF T/S=sub AND FAO_MOD=fine,very fine<br/> <math>\log_{10}(K_s) = 0.01</math></p> <p>Rule 3<br/> IF T/S=top AND FAO_MOD=coarse,fine,medium fine,organic,very fine<br/> <math>\log_{10}(K_s) = 1.14</math></p> <p>Rule 4<br/> IF T/S=top AND FAO_MOD=medium<br/> <math>\log_{10}(K_s) = 2.23</math></p>  |

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| (14) | $\log_{10}(K_s)$<br>/ $\log_{10}(\text{cm day}^{-1})$ | RT | <p>Rule 1<br/> IF <math>OC &lt; 0.96</math> AND <math>OC \geq 0.41</math> AND <math>FAO\_MOD = \text{coarse, medium, medium fine}</math><br/> <math>\log_{10}(K_s) = 1.54</math></p> <p>Rule 2<br/> IF <math>OC &lt; 0.40</math> AND <math>OC \geq 0.07</math> AND <math>FAO\_MOD = \text{medium, medium fine}</math><br/> <math>\log_{10}(K_s) = 1.30</math></p> <p>Rule 3<br/> IF <math>OC \geq 1.52</math> AND <math>OC &lt; 1.54</math> AND <math>T/S = \text{sub}</math><br/> <math>\log_{10}(K_s) = -0.75</math></p> <p>Rule 4<br/> IF <math>OC &lt; 0.40</math> AND <math>OC \geq 0.07</math> AND <math>FAO\_MOD = \text{coarse}</math><br/> <math>\log_{10}(K_s) = 1.83</math></p> <p>Rule 5<br/> IF <math>OC \geq 0.97</math> AND <math>OC &lt; 1.52</math> AND <math>T/S = \text{sub}</math><br/> <math>\log_{10}(K_s) = 1.13</math></p> <p>Rule 6<br/> IF <math>OC \geq 2.04</math> AND <math>OC &lt; 2.12</math> AND <math>T/S = \text{sub}</math><br/> <math>\log_{10}(K_s) = -0.58</math></p> <p>Rule 7<br/> IF <math>OC \geq 2.65</math> AND <math>OC &lt; 3.86</math> AND <math>T/S = \text{sub}</math><br/> <math>\log_{10}(K_s) = -0.45</math></p> <p>Rule 8<br/> IF <math>OC \geq 0.96</math> AND <math>OC &lt; 0.97</math> AND <math>T/S = \text{sub}</math> AND <math>FAO\_MOD = \text{fine, medium, medium fine}</math><br/> <math>\log_{10}(K_s) = -1.16</math></p> <p>Rule 9<br/> IF <math>OC &lt; 0.96</math> AND <math>OC \geq 0.41</math> AND <math>FAO\_MOD = \text{fine, very fine}</math><br/> <math>\log_{10}(K_s) = 0.79</math></p> <p>Rule 10<br/> IF <math>OC \geq 0.96</math> AND <math>OC &lt; 1.52</math> AND <math>T/S = \text{top}</math><br/> <math>\log_{10}(K_s) = 1.80</math></p> <p>Rule 11<br/> IF <math>OC \geq 0.40</math> AND <math>OC &lt; 0.41</math> AND <math>FAO\_MOD = \text{coarse}</math><br/> <math>\log_{10}(K_s) = -0.42</math></p> |
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Rule 12

IF OC>=3.86 AND T/S=sub

log<sub>10</sub>(K<sub>s</sub>)=0.37

Rule 13

IF OC>=2.10 AND T/S=top AND FAO\_MOD=coarse,medium

log<sub>10</sub>(K<sub>s</sub>)=1.19

Rule 14

IF OC< 0.07

log<sub>10</sub>(K<sub>s</sub>)=0.55

Rule 15

IF OC< 0.41 AND OC>=0.40 AND FAO\_MOD=fine,medium,medium fine,very fine

log<sub>10</sub>(K<sub>s</sub>)=-1.56

Rule 16

IF OC>=2.4 AND FAO\_MOD=fine,medium fine,organic,very fine

log<sub>10</sub>(K<sub>s</sub>)=-0.38

Rule 17

IF OC>=0.96 AND OC< 0.97 AND T/S=sub AND FAO\_MOD=coarse,very fine

log<sub>10</sub>(K<sub>s</sub>)=-0.44

Rule 18

IF OC>=1.54 AND OC< 2.04 AND T/S=sub

log<sub>10</sub>(K<sub>s</sub>)=1.33

Rule 19

IF OC< 0.40 AND OC>=0.07 AND FAO\_MOD=fine,very fine

log<sub>10</sub>(K<sub>s</sub>)=0.66

Rule 20

IF OC< 2.09 AND OC>=1.54 AND T/S=top

log<sub>10</sub>(K<sub>s</sub>)=1.74

Rule 21

IF OC>=2.12 AND OC< 2.65 AND T/S=sub

log<sub>10</sub>(K<sub>s</sub>)=1.29

Rule 22

IF OC>=2.09 AND OC< 2.10 AND T/S=top

log<sub>10</sub>(K<sub>s</sub>)=-0.87

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|      |   |    | <p>Rule 23<br/>IF OC&gt;=1.52 AND OC&lt; 1.54 AND T/S=top<br/>log<sub>10</sub>(K<sub>s</sub>)=-0.49</p> <p>Rule 24<br/>IF OC&gt;=2.10 AND OC&lt; 2.40 AND T/S=top AND FAO_MOD=fine,medium fine,organic,very fine<br/>log<sub>10</sub>(K<sub>s</sub>)=1.67</p>   |
| (15) | log <sub>10</sub> (K <sub>s</sub> ) / log <sub>10</sub> (cm day <sup>-1</sup> ) | RT | <p>Rule 1<br/>IF USDA=CL,L,LS,S,SiL,SL AND T/S=sub<br/>log<sub>10</sub>(K<sub>s</sub>)=0.82</p> <p>Rule 2<br/>IF USDA=C,O,SC,SCL,Si,SiC,SiCL<br/>log<sub>10</sub>(K<sub>s</sub>)=0.12</p> <p>Rule 3<br/>IF USDA=LS,S,SiL,SL AND T/S=top<br/>log<sub>10</sub>(K<sub>s</sub>)=1.47</p> <p>Rule 4<br/>IF USDA=CL,L AND T/S=top<br/>log<sub>10</sub>(K<sub>s</sub>)=2.69</p>  |
| (16) | log <sub>10</sub> (K <sub>s</sub> ) / log <sub>10</sub> (cm day <sup>-1</sup> ) | RT | <p>Rule 1<br/>IF OC&gt;=2.04 AND T/S=sub<br/>log<sub>10</sub>(K<sub>s</sub>)=-0.25</p> <p>Rule 2<br/>IF OC&lt; 0.40 AND OC&gt;=0.07 AND Sa&lt; 69.72 AND Sa&gt;=5.77<br/>log<sub>10</sub>(K<sub>s</sub>)=1.28</p> <p>Rule 3<br/>IF OC&lt; 0.96 AND OC&gt;=0.41 AND Cl&lt; 37.4<br/>log<sub>10</sub>(K<sub>s</sub>)=1.53</p> <p>Rule 4<br/>IF OC&gt;=1.52 AND OC&lt; 1.54 AND T/S=sub<br/>log<sub>10</sub>(K<sub>s</sub>)=-0.75</p> <p>Rule 5<br/>IF OC&gt;=0.96 AND OC&lt; 0.97 AND T/S=sub<br/>log<sub>10</sub>(K<sub>s</sub>)=-0.95</p> |

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|  |  | <p>Rule 6<br/>IF <math>OC \geq 0.97</math> AND <math>OC &lt; 1.52</math> AND <math>T/S = \text{sub}</math><br/><math>\log_{10}(K_s) = 1.13</math></p> <p>Rule 10<br/>IF <math>OC &lt; 0.40</math> AND <math>OC \geq 0.07</math> AND <math>S_a \geq 69.72</math><br/><math>\log_{10}(K_s) = 1.96</math></p> <p>Rule 11<br/>IF <math>OC \geq 0.40</math> AND <math>OC &lt; 0.41</math> AND <math>S_i &lt; 32.11</math><br/><math>\log_{10}(K_s) = -0.40</math></p> <p>Rule 12<br/>IF <math>OC &lt; 0.96</math> AND <math>OC \geq 0.41</math> AND <math>Cl \geq 37.4</math><br/><math>\log_{10}(K_s) = 0.67</math></p> <p>Rule 13<br/>IF <math>OC \geq 0.96</math> AND <math>OC &lt; 1.52</math> AND <math>T/S = \text{top}</math> AND <math>S_i \geq 10.85</math><br/><math>\log_{10}(K_s) = 1.82</math></p> <p>Rule 14<br/>IF <math>OC \geq 2.42</math> AND <math>T/S = \text{top}</math> AND <math>S_a &lt; 38.95</math><br/><math>\log_{10}(K_s) = -0.22</math></p> <p>Rule 15<br/>IF <math>OC &lt; 0.07</math><br/><math>\log_{10}(K_s) = 0.55</math></p> <p>Rule 16<br/>IF <math>OC &lt; 0.41</math> AND <math>OC \geq 0.40</math> AND <math>S_i \geq 32.11</math><br/><math>\log_{10}(K_s) = -1.81</math></p> <p>Rule 17<br/>IF <math>OC \geq 1.54</math> AND <math>OC &lt; 2.04</math> AND <math>T/S = \text{sub}</math><br/><math>\log_{10}(K_s) = 1.33</math></p> <p>Rule 18<br/>IF <math>OC \geq 1.54</math> AND <math>OC &lt; 2.09</math> AND <math>T/S = \text{top}</math> AND <math>S_i \geq 10.85</math><br/><math>\log_{10}(K_s) = 1.72</math></p> <p>Rule 19<br/>IF <math>OC \geq 2.10</math> AND <math>T/S = \text{top}</math> AND <math>S_a \geq 38.95</math><br/><math>\log_{10}(K_s) = 1.44</math></p> |
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|                                 |  |  | <p>Rule 20<br/>IF OC&gt;=2.09 AND OC&lt; 2.10 AND T/S=top<br/>log<sub>10</sub>(K<sub>s</sub>)=-0.87</p> <p>Rule 21<br/>IF OC&lt; 0.40 AND OC&gt;=0.07 AND Sa&lt; 5.77<br/>log<sub>10</sub>(K<sub>s</sub>)=-0.11</p> <p>Rule 22<br/>IF OC&gt;=1.52 AND OC&lt; 1.54 AND T/S=top AND Si&gt;=10.85<br/>log<sub>10</sub>(K<sub>s</sub>)=-0.46</p> <p>Rule 23<br/>IF OC&gt;=0.96 AND OC&lt; 2.09 AND T/S=top AND Si&lt; 10.85<br/>log<sub>10</sub>(K<sub>s</sub>)=0.01</p> <p>Rule 24<br/>IF OC&gt;=2.10 AND OC&lt; 2.42 AND T/S=top AND Sa&lt; 38.95<br/>log<sub>10</sub>(K<sub>s</sub>)=1.82</p>   |                                 |            |                |                                  |            |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|---------------------------------|--|--|--|---------------------------------|------------|----------------|----------------------------------|------------|--|--|--|--|--|--|---------------------------------|------------|------------|----------------------------------|------------|-----------|--------|-------|-------|--------|--------|--------|-------|---------|--------|-------|-------|--------|--------|--------|-------|---------|-------------|-------|-------|--------|--------|--------|------|---------|------|-------|-------|--------|--------|--------|-------|---------|-----------|-------|-------|--------|--------|--------|------|---------|-----------|---------|-------|-------|--------|--------|--------|------|--------|--------|-------|-------|--------|--------|--------|------|---------|--------|-------|-------|--------|--------|--------|-------|---------|-------------|-------|-------|--------|--------|--------|------|---------|------|-------|-------|--------|--------|--------|------|---------|--|-----------|-------|-------|--------|--------|--------|------|--------|--|---------|-------|-------|--------|--------|--------|-------|--------|
| (17)                            | log <sub>10</sub> (K <sub>s</sub> )<br>/ log <sub>10</sub> (cm day <sup>-1</sup> )                                 | LR   | log <sub>10</sub> K <sub>s</sub> = 0.4022 + 0.2612 * pH + 0.4456 * T/S - 0.02329 * CI - 0.01265 * Si - 0.01038 * CEC   |                                 |            |                |                                  |            |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
| (18)                            | MRC and HCC<br>( $\vartheta_r$ , $\vartheta_s$ , $\alpha$ , $n$ ,<br>$K_0$ , $L$<br>parameters<br>of MVG<br>model) | MS   | <table border="1"> <thead> <tr> <th colspan="2" rowspan="2">Modified FAO<br/>texture classes</th> <th colspan="7">MVG parameters</th> </tr> <tr> <th><math>\vartheta_r</math><br/>(cm<sup>3</sup> cm<sup>-3</sup>)</th> <th><math>\vartheta_s</math><br/>(cm<sup>3</sup> cm<sup>-3</sup>)</th> <th><math>\alpha</math><br/>(cm<sup>-1</sup>)</th> <th><math>n</math><br/>(-)</th> <th><math>m</math><br/>(-)</th> <th><math>K_0</math><br/>(cm day<sup>-1</sup>)</th> <th><math>L</math><br/>(-)</th> </tr> </thead> <tbody> <tr> <td rowspan="5">Top-soils</td> <td>coarse</td> <td>0.045</td> <td>0.438</td> <td>0.0478</td> <td>1.3447</td> <td>0.2563</td> <td>17.30</td> <td>-2.5587</td> </tr> <tr> <td>medium</td> <td>0.000</td> <td>0.459</td> <td>0.0309</td> <td>1.1920</td> <td>0.1611</td> <td>12.49</td> <td>-3.8570</td> </tr> <tr> <td>medium fine</td> <td>0.000</td> <td>0.432</td> <td>0.0094</td> <td>1.2119</td> <td>0.1749</td> <td>1.68</td> <td>-4.4460</td> </tr> <tr> <td>fine</td> <td>0.000</td> <td>0.478</td> <td>0.0403</td> <td>1.1176</td> <td>0.1053</td> <td>40.19</td> <td>-4.7040</td> </tr> <tr> <td>very fine</td> <td>0.000</td> <td>0.522</td> <td>0.0112</td> <td>1.1433</td> <td>0.1253</td> <td>2.69</td> <td>-5.0000</td> </tr> <tr> <td rowspan="5">Sub-soils</td> <td>organic</td> <td>0.111</td> <td>0.697</td> <td>0.0069</td> <td>1.4688</td> <td>0.3192</td> <td>1.42</td> <td>0.3284</td> </tr> <tr> <td>coarse</td> <td>0.057</td> <td>0.404</td> <td>0.0426</td> <td>1.5349</td> <td>0.3485</td> <td>9.68</td> <td>-1.8191</td> </tr> <tr> <td>medium</td> <td>0.000</td> <td>0.428</td> <td>0.0347</td> <td>1.1725</td> <td>0.1471</td> <td>11.78</td> <td>-4.9869</td> </tr> <tr> <td>medium fine</td> <td>0.000</td> <td>0.418</td> <td>0.0066</td> <td>1.2173</td> <td>0.1785</td> <td>1.87</td> <td>-3.3761</td> </tr> <tr> <td>fine</td> <td>0.000</td> <td>0.430</td> <td>0.0011</td> <td>1.2290</td> <td>0.1863</td> <td>0.07</td> <td>-1.8486</td> </tr> <tr> <td></td> <td>very fine</td> <td>0.000</td> <td>0.511</td> <td>0.0002</td> <td>1.4048</td> <td>0.2882</td> <td>0.02</td> <td>5.0000</td> </tr> <tr> <td></td> <td>organic</td> <td>0.000</td> <td>0.835</td> <td>0.0113</td> <td>1.2256</td> <td>0.1841</td> <td>10.81</td> <td>2.7337</td> </tr> </tbody> </table> | Modified FAO<br>texture classes |            | MVG parameters |                                  |            |  |  |  |  | $\vartheta_r$<br>(cm <sup>3</sup> cm <sup>-3</sup> ) | $\vartheta_s$<br>(cm <sup>3</sup> cm <sup>-3</sup> ) | $\alpha$<br>(cm <sup>-1</sup> ) | $n$<br>(-) | $m$<br>(-) | $K_0$<br>(cm day <sup>-1</sup> ) | $L$<br>(-) | Top-soils | coarse | 0.045 | 0.438 | 0.0478 | 1.3447 | 0.2563 | 17.30 | -2.5587 | medium | 0.000 | 0.459 | 0.0309 | 1.1920 | 0.1611 | 12.49 | -3.8570 | medium fine | 0.000 | 0.432 | 0.0094 | 1.2119 | 0.1749 | 1.68 | -4.4460 | fine | 0.000 | 0.478 | 0.0403 | 1.1176 | 0.1053 | 40.19 | -4.7040 | very fine | 0.000 | 0.522 | 0.0112 | 1.1433 | 0.1253 | 2.69 | -5.0000 | Sub-soils | organic | 0.111 | 0.697 | 0.0069 | 1.4688 | 0.3192 | 1.42 | 0.3284 | coarse | 0.057 | 0.404 | 0.0426 | 1.5349 | 0.3485 | 9.68 | -1.8191 | medium | 0.000 | 0.428 | 0.0347 | 1.1725 | 0.1471 | 11.78 | -4.9869 | medium fine | 0.000 | 0.418 | 0.0066 | 1.2173 | 0.1785 | 1.87 | -3.3761 | fine | 0.000 | 0.430 | 0.0011 | 1.2290 | 0.1863 | 0.07 | -1.8486 |  | very fine | 0.000 | 0.511 | 0.0002 | 1.4048 | 0.2882 | 0.02 | 5.0000 |  | organic | 0.000 | 0.835 | 0.0113 | 1.2256 | 0.1841 | 10.81 | 2.7337 |
| Modified FAO<br>texture classes |  | MVG parameters                                       |  |                                 |            |                |                                  |            |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 |  | $\vartheta_r$<br>(cm <sup>3</sup> cm <sup>-3</sup> ) | $\vartheta_s$<br>(cm <sup>3</sup> cm <sup>-3</sup> )   | $\alpha$<br>(cm <sup>-1</sup> ) | $n$<br>(-) | $m$<br>(-)     | $K_0$<br>(cm day <sup>-1</sup> ) | $L$<br>(-) |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
| Top-soils                       | coarse   | 0.045  | 0.438  | 0.0478                          | 1.3447     | 0.2563         | 17.30                            | -2.5587    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | medium   | 0.000  | 0.459  | 0.0309                          | 1.1920     | 0.1611         | 12.49                            | -3.8570    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | medium fine  | 0.000  | 0.432  | 0.0094                          | 1.2119     | 0.1749         | 1.68                             | -4.4460    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | fine   | 0.000  | 0.478  | 0.0403                          | 1.1176     | 0.1053         | 40.19                            | -4.7040    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | very fine  | 0.000  | 0.522  | 0.0112                          | 1.1433     | 0.1253         | 2.69                             | -5.0000    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
| Sub-soils                       | organic  | 0.111  | 0.697  | 0.0069                          | 1.4688     | 0.3192         | 1.42                             | 0.3284     |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | coarse   | 0.057  | 0.404  | 0.0426                          | 1.5349     | 0.3485         | 9.68                             | -1.8191    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | medium   | 0.000  | 0.428  | 0.0347                          | 1.1725     | 0.1471         | 11.78                            | -4.9869    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | medium fine  | 0.000  | 0.418  | 0.0066                          | 1.2173     | 0.1785         | 1.87                             | -3.3761    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | fine   | 0.000  | 0.430  | 0.0011                          | 1.2290     | 0.1863         | 0.07                             | -1.8486    |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | very fine  | 0.000  | 0.511  | 0.0002                          | 1.4048     | 0.2882         | 0.02                             | 5.0000     |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 | organic  | 0.000  | 0.835  | 0.0113                          | 1.2256     | 0.1841         | 10.81                            | 2.7337     |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
| (19)                            | MRC and HCC<br>( $\vartheta_r$ , $\vartheta_s$ , $\alpha$ , $n$ ,<br>$K_0$ , $L$                                   | MS   | <table border="1"> <thead> <tr> <th colspan="2" rowspan="2">USDA texture<br/>classes</th> <th colspan="7">MVG parameters</th> </tr> <tr> <th><math>\vartheta_r</math></th> <th><math>\vartheta_s</math></th> <th><math>\alpha</math></th> <th><math>n</math></th> <th><math>m</math></th> <th><math>K_0</math></th> <th><math>L</math></th> </tr> </thead> <tbody> </tbody> </table>   | USDA texture<br>classes         |            | MVG parameters |                                  |            |  |  |  |  | $\vartheta_r$  | $\vartheta_s$  | $\alpha$                        | $n$        | $m$        | $K_0$                            | $L$        |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
| USDA texture<br>classes         |  | MVG parameters                                       |  |                                 |            |                |                                  |            |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |
|                                 |  | $\vartheta_r$  | $\vartheta_s$  | $\alpha$                        | $n$        | $m$            | $K_0$                            | $L$        |  |  |  |  |  |  |                                 |            |            |                                  |            |           |        |       |       |        |        |        |       |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |       |         |           |       |       |        |        |        |      |         |           |         |       |       |        |        |        |      |        |        |       |       |        |        |        |      |         |        |       |       |        |        |        |       |         |             |       |       |        |        |        |      |         |      |       |       |        |        |        |      |         |  |           |       |       |        |        |        |      |        |  |         |       |       |        |        |        |       |        |

|      | parameters of MVG model)  |   |   |                 | (cm <sup>3</sup> cm <sup>-3</sup> ) | (cm <sup>3</sup> cm <sup>-3</sup> ) | (cm <sup>-1</sup> ) | (-)    | (-)    | (cm day <sup>-1</sup> ) | (-)     |
|------|---|---|---|-----------------|-------------------------------------|-------------------------------------|---------------------|--------|--------|-------------------------|---------|
|      |   |   |   |                 |                                     |                                     |                     |        |        |                         |         |
|      |   |   | Top-soils   | sand            | 0.061                               | 0.411                               | 0.0258              | 1.8005 | 0.4446 | 8.33                    | -0.7306 |
|      |   |   |   | loamy sand      | 0.052                               | 0.475                               | 0.0341              | 1.4846 | 0.3264 | 8.95                    | -1.8749 |
|      |   |   |   | sandy loam      | 0.000                               | 0.441                               | 0.0750              | 1.1904 | 0.1599 | 44.88                   | -4.3523 |
|      |   |   |   | loam            | 0.000                               | 0.491                               | 0.0347              | 1.1931 | 0.1618 | 14.17                   | -4.3000 |
|      |   |   |   | silt loam       | 0.000                               | 0.424                               | 0.0074              | 1.2545 | 0.2029 | 1.17                    | -3.5496 |
|      |   |   |   | silt            | 0.009                               | 0.465                               | 0.0042              | 1.4853 | 0.3267 | 1.38                    | -2.6418 |
|      |   |   |   | sandy clay loam | 0.000                               | 0.409                               | 0.0700              | 1.1335 | 0.1178 | 43.63                   | -5.0000 |
|      |   |   |   | clay loam       | 0.000                               | 0.465                               | 0.1284              | 1.1160 | 0.1040 | 195.15                  | -5.0000 |
|      |   |   |   | silty clay loam | 0.000                               | 0.463                               | 0.0107              | 1.1892 | 0.1591 | 1.38                    | -2.6418 |
|      |   |   |   | sandy clay      | 0.192                               | 0.523                               | 0.0351              | 1.4455 | 0.3082 | 43.80                   | -1.6202 |
|      |   |   |   | silty clay      | 0.000                               | 0.455                               | 0.0309              | 1.1110 | 0.0999 | 0.01                    | 5.0000  |
|      |   |   |   | clay            | 0.000                               | 0.499                               | 0.0234              | 1.1200 | 0.1072 | 17.07                   | -5.0000 |
|      |   |   |   | organic         | 0.111                               | 0.697                               | 0.0069              | 1.4688 | 0.3192 | 1.42                    | 0.3284  |
|      |   |   | Sub-soils   | sand            | 0.034                               | 0.368                               | 0.0356              | 1.7767 | 0.4372 | 5.97                    | -1.4096 |
|      |   |   |   | loamy sand      | 0.037                               | 0.423                               | 0.0419              | 1.4222 | 0.2968 | 14.84                   | -1.9583 |
|      |   |   |   | sandy loam      | 0.000                               | 0.437                               | 0.0681              | 1.1966 | 0.1643 | 53.50                   | -3.7279 |
|      |   |   |   | loam            | 0.000                               | 0.432                               | 0.0336              | 1.1701 | 0.1454 | 8.58                    | -5.0000 |
|      |   |   |   | silt loam       | 0.000                               | 0.422                               | 0.0077              | 1.2483 | 0.1989 | 1.76                    | -3.3247 |
|      |   |   |   | silt            | 0.009                               | 0.465                               | 0.0042              | 1.4853 | 0.3267 | 0.45                    | -5.0000 |
|      |   |   |   | sandy clay loam | 0.000                               | 0.384                               | 0.0717              | 1.1206 | 0.1076 | 37.09                   | -5.0000 |
|      |   |   |   | clay loam       | 0.000                               | 0.413                               | 0.0227              | 1.1191 | 0.1064 | 12.35                   | -5.0000 |
|      |   |   |   | silty clay loam | 0.000                               | 0.408                               | 0.0032              | 1.1993 | 0.1662 | 0.45                    | -5.0000 |
|      |   |   |   | sandy clay      | 0.000                               | 0.365                               | 0.0016              | 1.1812 | 0.1534 | 43.80                   | -1.6202 |
|      |   |   |   | silty clay      | 0.000                               | 0.442                               | 0.0003              | 1.3861 | 0.2786 | 0.01                    | 5.0000  |
|      |   |   |   | clay            | 0.000                               | 0.461                               | 0.0004              | 1.3027 | 0.2323 | 0.04                    | 1.1840  |
|      |   |   |   | organic         | 0.000                               | 0.835                               | 0.0113              | 1.2256 | 0.1841 | 10.81                   | 2.7337  |
| (20) | MRC ( $\vartheta_r$ / cm <sup>3</sup> cm <sup>-3</sup> , $\vartheta_s$ / cm <sup>3</sup> cm <sup>-3</sup> , log <sub>10</sub> ( $\alpha$ ) / log <sub>10</sub> (cm <sup>-1</sup> ), log <sub>10</sub> (n-1) / - parameters of VG model) | RT (for $\vartheta_r$ ) and LRt (for $\vartheta_s$ , log <sub>10</sub> ( $\alpha$ ) and log <sub>10</sub> ( $\alpha$ )) | <p>Rule 1<br/>IF <math>S_a \geq 2.00</math><br/><math>\theta_r = 0.041</math></p> <p>Rule 2<br/>IF <math>S_a &lt; 2.00</math><br/><math>\theta_r = 0.179</math></p> <p><math>\theta_s = 0.5056 - 0.1437 * (1/(OC+1)) + 0.0004152 * Si</math><br/> <math>log_{10}(\alpha) = -1.3048 - 0.0006123 * Si - 0.009810 * Cl + 0.07611 * Si * Cl - 0.0004508 * (1/(OC+1)) + 0.03472 * Cl * (1/(OC+1)) - 0.01226 * Si * (1/(OC+1))</math><br/> <math>log_{10}(n-1) = 0.01516 - 0.005775 * (1/(OC+1)) - 0.2488 * log_{10}(CEC) - 0.01918 * Cl - 0.0005052 * Cl * (1/(OC+1)) - 0.007544 * Cl * log_{10}(CEC) - 0.02159 * Si + 0.01556 * (1/(OC+1)) * pH^2 + 0.01477 * pH^2 + 0.0001121 * Si * Cl - 0.3320 * (1/(OC+1)) * log_{10}(CEC)</math></p> |                 |                                     |                                     |                     |        |        |                         |         |

|      |   |   |   |
|------|---|---|---|
| (21) | MRC ( $\theta_r / \text{cm}^3$ , $\theta_s / \text{cm}^3$ , $\log_{10}(\alpha) / \log_{10}(\text{cm}^{-1})$ , $\log_{10}(n-1)$ / - parameters of VG model)  | RT (for $\theta_r$ ) and LR (for $\theta_s$ , $\log_{10}(\alpha)$ and $\log_{10}(\alpha)$ )   | <p>Rule 1<br/>IF Sa &gt;= 2.00<br/><math>\theta_r = 0.041</math></p> <p>Rule 2<br/>IF Sa &lt; 2.00<br/><math>\theta_r = 0.179</math></p> <p><math>\theta_s = 0.8308 - 0.2822 * \text{BD} + 0.0002728 * \text{Cl} + 0.0001869 * \text{Si}</math><br/> <math>\log_{10}(\alpha) = -0.4335 - 0.4173 * \text{BD} - 0.04762 * \text{OC} + 0.2181 * \text{T/S} - 0.01581 * \text{Cl} - 0.01207 * \text{Si}</math><br/> <math>\log_{10}(n-1) = 0.2224 - 0.3019 * \text{BD} - 0.05558 * \text{T/S} - 0.005306 * \text{Cl} - 0.003084 * \text{Si} - 0.01072 * \text{OC}</math></p>                            |
| (22) | MRC ( $\theta_r$ ( $\text{cm}^3 \text{cm}^{-3}$ ), $\theta_s$ ( $\text{cm}^3 \text{cm}^{-3}$ ), $\log_{10}(\alpha)$ ( $\log_{10}(\text{cm}^{-1})$ ), $\log_{10}(n-1)$ (-) parameters of VG model) | RT (for $\theta_r$ ) and LRT2 (for $\theta_s$ , $\log_{10}(\alpha)$ and $\log_{10}(\alpha)$ ) | <p>Rule 1<br/>IF Sa &gt;= 2.00<br/><math>\theta_r = 0.041</math></p> <p>Rule 2<br/>IF Sa &lt; 2.00<br/><math>\theta_r = 0.179</math></p> <p><math>\theta_s = 0.6305 - 0.1026 * \text{BD}^2 + 0.0002904 * \text{pH}^2 + 0.0003335 * \text{Cl}</math><br/> <math>\log_{10}(\alpha) = -1.1652 + 0.4051 * (1/(\text{OC}+1)) - 0.1606 * \text{BD}^2 - 0.008372 * \text{Cl} - 0.01300 * \text{Si} + 0.002166 * \text{pH}^2 + 0.08233 * \text{T/S}</math><br/> <math>\log_{10}(n-1) = -0.2593 + 0.2568 * (1/(\text{OC}+1)) - 0.1059 * \text{BD}^2 - 0.009004 * \text{Cl} - 0.001223 * \text{Si}</math></p> |

<sup>a</sup>Abbreviations used in table: FAO\_MOD: modified FAO texture classes (5 class for mineral soils and an organic class); USDA: USDA-SCS texture classes and an organic class (S: sand, LS: loamy sand, SL: sandy loam, L: loam, SiL: silt loam, Si: silt, SCL: sandy clay loam, CL: clay loam, SiCL: silty clay loam, SC: sandy clay, SiC: silty clay, C: clay, O: organic soils); Sa: sand content (50-2000  $\mu\text{m}$ ) (%); Si: silt content (2-50  $\mu\text{m}$ ) (%); Cl: clay content (0-2  $\mu\text{m}$ ) (%); T/S: top-soil (top) and sub-soil (sub) distinction; OC: organic carbon content (%); BD: bulk density ( $\text{g cm}^{-3}$ ); pH: pH in water; CEC: cation exchange capacity ( $\text{meq } 100\text{g}^{-1}$ );  $\theta_s$ : saturated water content ( $\text{cm}^3 \text{cm}^{-3}$ );  $\theta_{FC}$ : water content at field capacity ( $\text{cm}^3 \text{cm}^{-3}$ );  $\theta_{WP}$ : water content at wilting point ( $\text{cm}^3 \text{cm}^{-3}$ );  $K_s$ : saturated hydraulic conductivity ( $\log_{10}(\text{cm day}^{-1})$ ); MRC: moisture retention curve; HCC: hydraulic conductivity curve; VG: van Genuchten model; MVG: Mualem-van Genuchten model; MS: mean statistics of developer determined groups; RT: univariate regression tree; LR, LRT, LRT2: linear regression with or without transformation and interactions, further details of the LR models are provided in 'Basic principles for fitting the linear regression (LR) model' section.